

Original article

Modeling for reorientation and potential of enhanced oil recovery in refracturing

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Abstract:

Reorientation of fractures and high production improvement are observed and illustrated by fields and theoretical researches. During the refracturing treatments, it is important to get familiar with the enhanced oil recovery mechanics of fracture reorientation and distribution of residual oil. Mechanisms of fracture reorientation are discussed in order to design the parameters of reoriented fractures in numerical simulation. To further evaluate the oil recovery of different angles of reoriented fractures, geological and numerical models are simulated using data of the actual reservoir with rhombus inverted nine spot well pattern, different angles of reoriented fracture are designed for both corner and edge wells to obtain the enhanced oil recovery. Results show that potential of production increase is highly impacted by the well pattern and angles of fractures and meanwhile impacted by distribution of residual oil and formation properties. Oil enhancement potential is significantly different with fracture reorientation angles in refracturing treatment: cumulative produced oil for corner wells is symmetrical around the angle of 0° and reaches the highest at the angles of positive and negative 23°; for the edge wells, it is also symmetrical around the angle of 0° while reaches the highest cumulative oil at the angles of positive and negative 90°. The difference shows that optimal angles exist for reoriented fractures during refracturing design and with proper induced reoriented fractures, more oil will be recovered for field restimulation treatments.

1. Introduction

Well production will decrease due to lose of flow conductivity in the initial fractures after fracturing treatment (Sallee and Rugg, 1953; Hubbert and Willis, 1972). Refracturing treatment is one of the most effective restimulation technique to regain or enhance production in those wells after long-term development, it is announced that the estimated ultimate recovery (EUR) could be increased by 53% in the Eagleford and by 69% in the Bakken after refracturing treatment (Preiksaitis et al., 2016; Shah et al., 2017). There are three main purposes of refracturing treatment in order to increase the EUR, reopening the initial fractures and injecting more proppant to restore the flow capacity, improving the fracture geometry of the initial fractures to reach far field residual oil, and inducing fracture reorientation to connect the by-passed pay zones in reservoirs (Elbel and Mack, 1993; Vincent, 2011).

Oil recovery will be boosted if fractures are reoriented in refracturing treatment since more residual oil will be mobilized and high pressure region will be intersected. After being monitored in field tests, fracture reorientation has been a research hotspot due to its high production enhancement. In situ stress field alternation is the main reason that leads to fracture reorientation in refracturing treatment (Warpinski and Branagan, 1989; Zhang and Chen, 2010; Roussel and Sharma, 2012). New fractures will initiate and propagate to the perpendicular direction of the initial fractures which is observed in both vertical wells (Siebrits et al., 1998; Roussel and Sharma, 2010) and horizontal wells (Roussel and Sharma, 2011; Barree et al., 2017). In water flooding reservoirs, water injection and underground liquid withdrawn will lead to pressure gradient of formation and then impact the in situ stress field (Berchenko and Detournay, 1997). Stress reversal region will be formed with stress field alternation and



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it is applied to determine the fracture reoriented distance in refracturing treatment (Warpinski et al., 1982; Dahi-Taleghani and Olson, 2011). Many researches have been done on stress field change after initial fracturing to verify the exist of fracture reorientation. Two contributors for stress reorientation are then presented: mechanical and poroelastic effects. The mechanical effect results from the opening of a propped fracture and the poroelastic effect results from pore pressure change while producing underground liquid. This theory was applied and two dimensionless parameters were presented to identify if fracture reorientation happens in refracturing treatment (Roussel and Sharma, 2013). Meanwhile, fracture reorientation can be induced by right fracturing techniques and methods (Ishida et al., 2019). It is found that perforation is an important factor to determine the direction of reorientation, perforation orientation affects the propagation reorientation in refracturing, and the shape of new fracture is affected by perforation orientation and differential stress at the same time (Zhang et al., 2008; Zhang and Chen, 2010; Guo et al., 2018). With literature reviews, some researchers worked on fracture reorientation and production analysis after refracturing (Zhang and Chen, 2009a, 2009b). Numerical and analytical models are built to calculate stress field and predict production after refracturing treatment. Factors influenced the production after refracturing treatment are analyzed, and it is identified that production will be increased by clearly analyzing the processes of fracturing treatment and production. Many of the former presented models are not suitable for predicting production of complicated fractures, especially in wells that fracture initiates and propagates at the direction different with the initial one (Reeves et al., 1999).

Many researchers have done excellent work to promote the development of refracturing technology (Bratov, 2018; Teng et al., 2019). Most researches are emphasized on the mechanics

of enhanced oil recovery in refracturing, stresses analysis before refracturing and fractures propagation determination after refracturing. However, not enough detailed researches are published on evaluating potential of enhanced oil recovery in refracturing design, especially potential at different angles of the reoriented fractures. In this paper, enhanced oil recovery potential of the reoriented fractures at different angles is discussed based on the actual field data and influenced factors will be analyzed. Optimal designs of induced fracture reorientation will be proposed for field engineers.

2. Discussion of fracture reorientation

2.1 Basic theory of fracture reorientation

Fractures created in refracturing treatment may differ with the original azimuth and dip angle under some conditions, which is identified as fracture reorientation. The two main reasons for this are: propped initial fracture causes stress filed alternation around the fracture, and pore pressure change due to underground liquid production alters the initial stress field around the fracture, which are identified as mechanical effect and poroelastic effect, respectively. As shown in Fig. 1 (Lolon et al., 2008; Zhang and Chen, 2010), stress reversal caused by mechanical effect can be explained by the increase of both minimum and maximum horizontal stress due to the existing of propped fracture. However, it is obviously that stress at the direction perpendicular to the fracture increases more than that at the direction parallel to the fracture. At the original stress field, maximum horizontal stress is parallel to the initial fracture, but if the stress differential between the maximum and minimum horizontal stress is small enough and the stress increase at the direction of minimum horizontal stress is more than that at the direction of maximum horizontal stress, the minimum horizontal stress will exceed the maximum horizontal stress

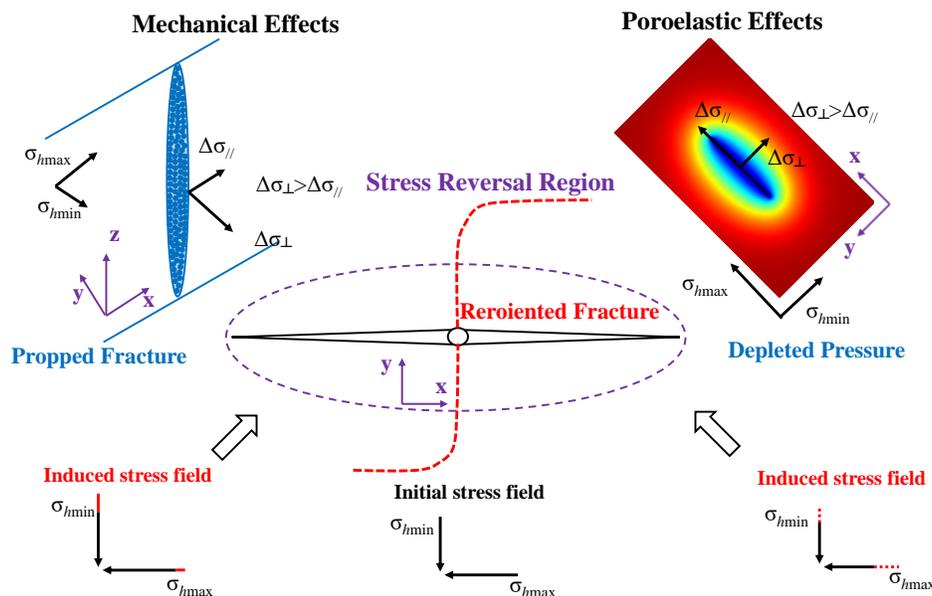


Fig. 1. Stress reversal caused by mechanical and poroelastic effects.

which will cause that direction of horizontal stresses reverse at the angle of 90° around the fracture that is called stress reversal region. Similarly, stress reversal caused by poroelastic effect can be explained that pore pressure drops more at the direction parallel to the fracture than that perpendicular to the fracture with underground liquid produced, which will lead to decrease of maximum horizontal stress faster than that of minimum horizontal stress. Finally, the minimum horizontal stress will exceed the maximum horizontal stress. Stress alternation can be induced by both mechanical effect and poroelastic effect, and stress reversal region will exist more easily especially with small stress differential between initial maximum and minimum horizontal stress.

As shown in Fig. 2, because the direction of the maximum horizontal stress is oriented by 90° around the fracture, fracture created in refracturing will initiate at the direction perpendicular to the initial fracture and propagate to the isotropic point where the maximum horizontal stress equals to the minimum horizontal stress. After that, fracture will change direction gradually to the direction of the initial fracture because direction of stresses won't change at far field.

2.2 Feasibility analysis of fracture reorientation

2.2.1 Criteria of fracture reorientation

Normally, it is difficult to evaluate or predict whether fracture will reorient in refracturing treatment because it needs huge amounts of work in numerical simulation as well as physical simulation. However, there is still some excellent works from researchers provide simple and operable methods for usage in fields. Here, two dimensionless criteria (Zhang and Chen, 2010) are discussed and applied in actual field samples. The two criteria can reveal mechanical effect and poroelastic effect to a certain extent and help to identify the possibility of fracture reorientation.

The first criterion is named as mechanical stress reorientation number, expressed as Eq. (1), which is defined as the ratio of the in-situ stress contrast and the net closing pressure of a propped fracture. The second criterion is named as poroelastic stress reorientation number, which is expressed as Eq. (2) and defined as the ratio of the in-situ stress contrast and the stress contrast generated by the pore pressure gradients.

$$\Pi_{mech} = \frac{\sigma_{hmax} - \sigma_{hmin}}{P_c - \sigma_{hmin}} = \frac{\Delta\sigma_h}{P_{net}} \quad (1)$$

$$\Pi_{pore} = \frac{\sigma_{hmax} - \sigma_{hmin}}{\sigma_*} = \frac{\Delta\sigma_h}{\frac{\alpha(1-2\gamma)}{1-\gamma}(P_{Ri} - P_{wf})} \quad (2)$$

where Π_{mech} is the mechanical stress reorientation number; Π_{pore} is poroelastic stress reorientation number; σ_{hmax} , σ_{hmin} is maximum and minimum horizontal stress, MPa; $\Delta\sigma_h$ is horizontal stress contrast, MPa; σ_* is stress contrast generated by pore pressure gradients, MPa; P_{Ri} is initial reservoir pressure, MPa; P_{wf} is bottomhole pressure, MPa; γ is Poisson's ratio; α is Biot's constant; and $P_{net} = P_c - \sigma_{hmin}$ can be expressed as Eq. (3) which is defined as net fracture closure pressure, MPa.

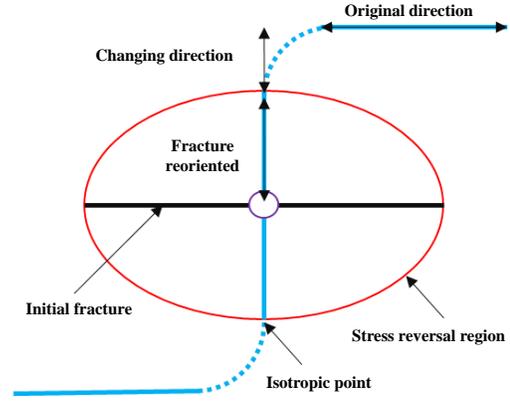


Fig. 2. Geometry of stress reversal region and refracture propagation direction.

$$P_{net} = \frac{EW_f}{2(1-\gamma^2)h} \quad (3)$$

where E is Young's modulus, MPa; h is formation thickness, m; W_f is fracture width, m.

These two criteria help to quantify the potential for the propagation of orthogonal refracturing in a given field. Also, the possible value of stress reorientation is identified as below 0.1 for both criteria.

2.2.2 Fracture reorientation of field sample

The criteria above are used to quantify the potential for fracture reorientation by applying data of actual oilfield. All data is obtained at 4 years after wells opening, and about 200 wells of the target reservoir are summarized with the two criteria calculated as shown as Figs. 3 and 4.

By comparing the two stress reorientation numbers, it can be indicated that poroelastic stress reorientation numbers are all above 0.1 which means that it is difficult to induce stress reversal by porosity drop around initial fracture. However, it doesn't mean that poroelastic effect won't lead to fracture reorientation in this reservoir, because the producing wells are just put into production for 4 years, when reservoir pressure and pore pressure are still not so depleted for inducing stress reversal. Meanwhile, it shows that mechanical stress reorientation numbers of some wells are less than 0.1, which

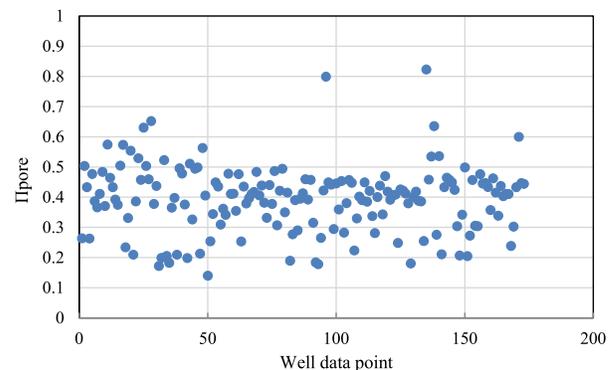


Fig. 3. Distribution of mechanical stress reorientation numbers.

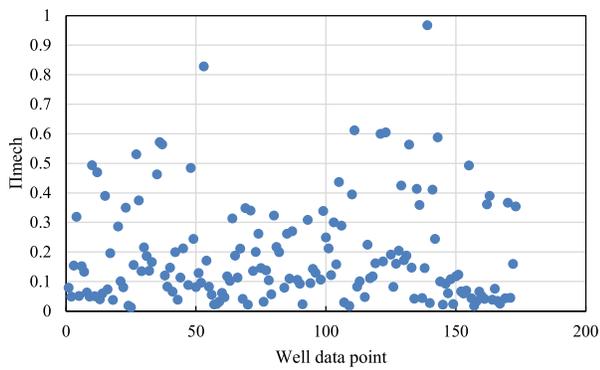


Fig. 4. Distribution of poroelastic stress reorientation numbers.

means possible fracture reorientation in refracturing treatment and indicates that mechanical effect may be the dominant effect for reorientation in this reservoir.

3. Numerical simulation of fracture reorientation and refracturing

3.1 Basic model and parameters

Actual data of field wells are collected for numerical simulation, and targeted field is a typical low permeability sandstone reservoir with rhombus inverted nine spot well pattern. In order to focus well interference on the researched wells, trick is played in choosing well for numerical simulation, as shown in Fig. 5. P3 is an edge well and P5 is a corner well, both of which are target wells for detailed research. All wells will be fractured before opening, while the two target wells will be refractured after 4 years separately to evaluate the potential of enhanced oil recovery. Size of model is $1000\text{ m} \times 600\text{ m} \times 6\text{ m}$, and number of grids is $100 \times 60 \times 6$.

After analyzing the initial stress field, direction of the maximum horizontal well is $\text{NE}67^\circ$. So the grids of the numerical model are rotated to make sure that the maximum horizontal stress is parallel to the X axis. Other basic parameters are shown as Table 1.

Relative permeability curve applied in the numerical model is shown as Fig. 6.

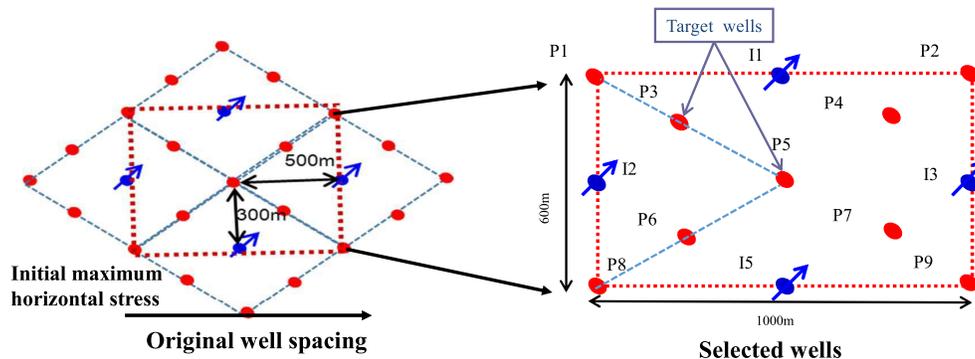


Fig. 5. Target wells for reorientation design and potential evaluation.

Thus, dynamic data can be calculated by the established numerical simulation model, and prediction of producing data of each well can be obtained every month. Based on the modeling results, some detailed discussion will be conducted in next sections.

Table 1. Basic model parameters.

Parameter	Unit	Value
Porous media density	kg/m^3	2500
Dead oil density	kg/m^3	851
Average permeability	μm^2	0.002
Average effective porosity	-	0.125
Initial reservoir pressure	MPa	10
Saturated pressure	MPa	6.85
Oil formation volume factor	-	1.206
Bottomhole pressure	MPa	5
Underground oil viscosity	$\text{mPa}\cdot\text{s}$	2.24
Reservoir depth	m	1580
Liquid compressibility factor	MPa^{-1}	1.05×10^{-4}
Porous media compressibility factor	MPa^{-1}	2.0×10^{-4}
Formation water compressibility factor	MPa^{-1}	1.0×10^{-4}

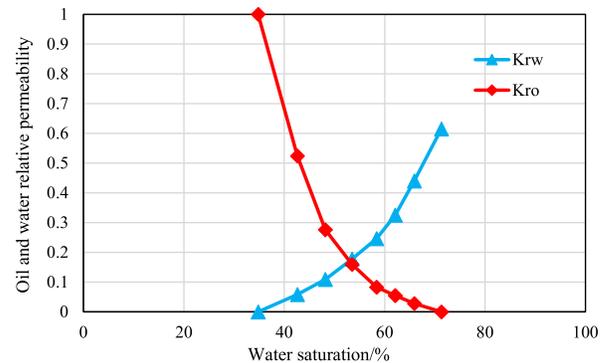


Fig. 6. Relative permeability curve.

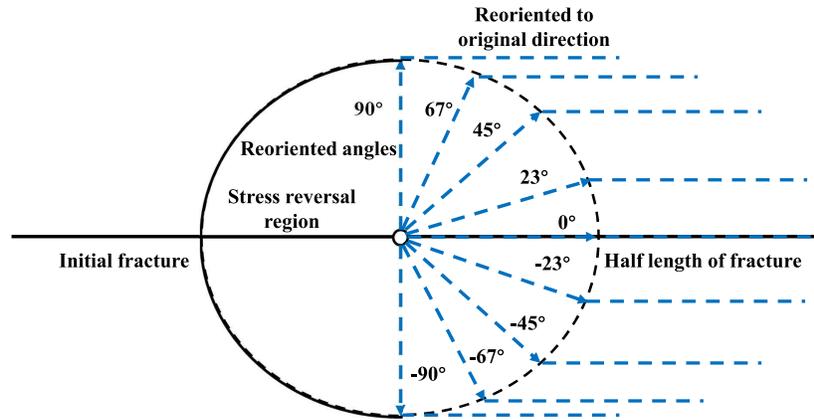


Fig. 8. Geometry of stress reversal region and fracture propagation.

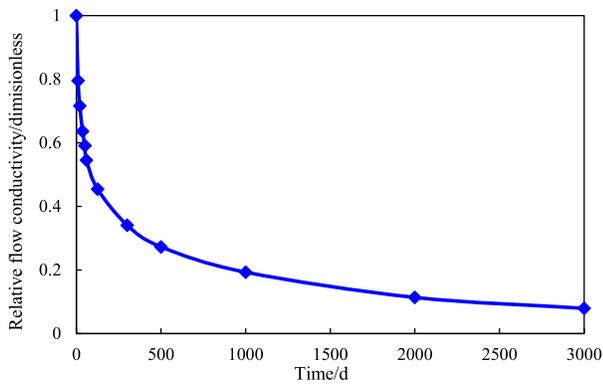


Fig. 7. Relationship of relative flow conductivity of fracture versus time.

3.2 Simulation of reoriented fractures

Initial fractures are simulated with the method of local grid refinement with fracture half-length of 150 m and initial fracture conductivity of $150 \times 10^{-3} \mu\text{m}^2\cdot\text{m}$. And since flow capacity will decrease with time, flow conductivity is set to change with time in the numerical simulation model. Eq. (4) shows the relationship of relative flow conductivity of fracture versus time and can be plot as Fig. 7.

$$K_f w_f = K_{f0} w_0 [1 - 0.271g(t + 1)] \quad (4)$$

where $K_{f0} w_0$ is the initial flow conductivity, $10^{-3} \mu\text{m}^3$; t is time, day.

After developing for 4 years, refracturing treatment will be completed to the targeted researching corner well and edge well. As illustrated above, there is high possibility that fracture will be reoriented after refracturing, and geometry of reoriented fractures is simplified as show in Fig. 8. The stress reversal region is assumed as a circle instead of an ellipse, fractures initiate from the wellbore perpendicular to the initial fracture and propagate directly to the isotropic point, and then the process that fracture reorients to the initial fracture is eliminated due to the its short propagation path. All the simplifications are based on that fracture propagation during

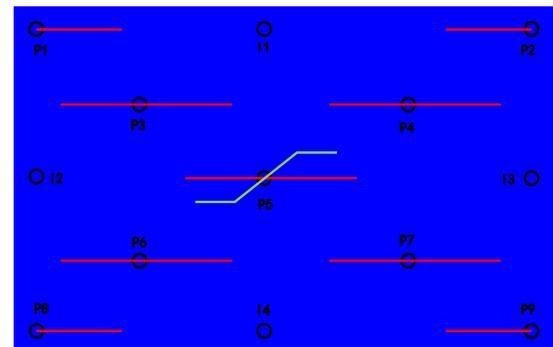


Fig. 9. Schematic of fracture in simulation (corner well 45°).

refracturing is not the priority thing researched in this paper, and the most important thing is to figure out the potential of enhanced oil recovery with reoriented fractures of different angles. As discussed by Zhang and Chen (2010), fractures can be reoriented to fixed direction as the operators wished which is verified and simulated in physical experiments, and angles of oriented fractures designed in this paper are set as some fixed values as shown in Fig. 8.

Simulation of reoriented fractures in the model is shown as Fig. 9. Take the corner well with fracture reorientation angle of 45° as the sample. And it is assumed that fractures will restore flow conductivity to the initial level, and then it decreases following the relationship of relative flow conductivity of fracture versus time.

4. Analysis of residual oil distribution in refracturing

4.1 Residual oil distribution of corner well

Fig. 10 shows distribution of residual oil saturation under different conditions of the target corner well. Fig. 10(a) is distribution of residual oil saturation of the 4th year, and no refracturing treatment is completed yet. Fig. 10(b) shows distribution of residual oil saturation of the 10th year with no refracturing treatment. Fig. 10(c) shows distribution of residual

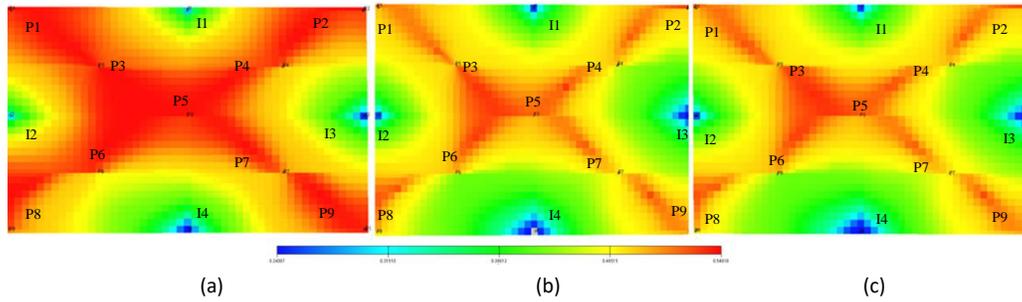


Fig. 10. Residual oil saturation of the corner well, (a) 4th year before refracturing, (b) the 10th year without refracturing, (c) the 10th year, refracturing at the 4th year without fracture reorientation.

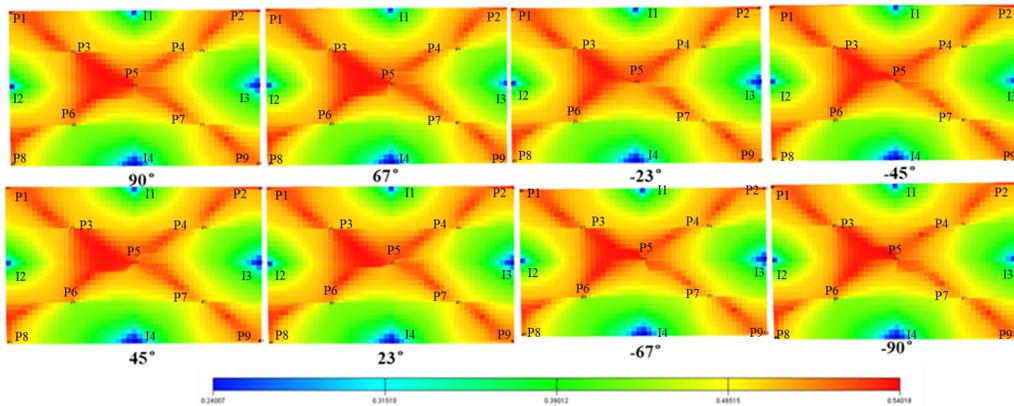


Fig. 11. Oil saturation with different angles of fracture reorientation after refracturing (corner well).

oil saturation of the 10th year with refracturing treatment completed at the 4th producing year with no fracture reorientation in the refracturing treatment.

It is obviously that residual oil saturation is much lower at the 10th year than that at the 4th year development as shown in Fig. 10(a) and Fig. 10(b). However, there seems to be no big difference of residual oil saturation between Fig. 10(b) and Fig. 10(c), and restore the conductivity of the initial fracture can increase the production while the enhancement is limited because there is not enough residual oil around the initial fracture and pore pressure drops too much, which all determine that potential of enhanced oil recovery of reopening initial fracture is lower than fracture reorientation. Meanwhile, most of the residual oil is remained at all four corner point of the drainage area of the corner well, to enhance the oil recovery, to motivate the residual oil and there is the most effective way.

Refracturing treatment is implemented after producing with the initial fracture for 4 years when fracture conductivity of the initial fracture has already dropped to less than 20% of the original value or even worse of losing all the conductivity. Fractures initiated in the refracturing treatment are design with different angles of reorientation including 90°, 67°, 45°, 23°, -23°, -45°, -67°, -90° as illustrated in Fig. 8. Also, 0° with refracturing treatment but no fracture orientation was discussed above. Residual oil saturation of the target corner well with different angles of fracture reorientation after refracturing is shown as Fig. 11. Distribution of residual oil with different

angles is obviously different which indicates that regions with more residual oil can be intersected by fracture reorientation.

4.2 Residual oil distribution of edge well

Same as the corner well, distribution of residual oil saturation under different conditions of the target edge well is also depicted as shown in Fig. 12. Similarly, Fig. 12(a) is for the 4th year with no refracturing treatment, Fig. 12(b) is for the 10th year with no refracturing treatment, and Fig. 12(c) is for the 10th year with refracturing treatment completed at the 4th producing year and no fracture reorientation in the refracturing treatment.

Similarly, fractures are design with different angles of reorientation including 90°, 67°, 45°, 23°, -23°, -45°, -67°, -90°. Residual oil saturation of the target edge well with different angles of fracture reorientation after refracturing is shown as Fig. 13. Influence of fracture angles of edge well seems to be larger than that of the corner well. Also, it is shown that region with rich residual oil of edge well is narrower than that of the corner well because wells at different positions are varied in drainage areas.

5. Enhanced oil recovery analysis of fracture reorientation

5.1 Enhanced oil recovery of corner well

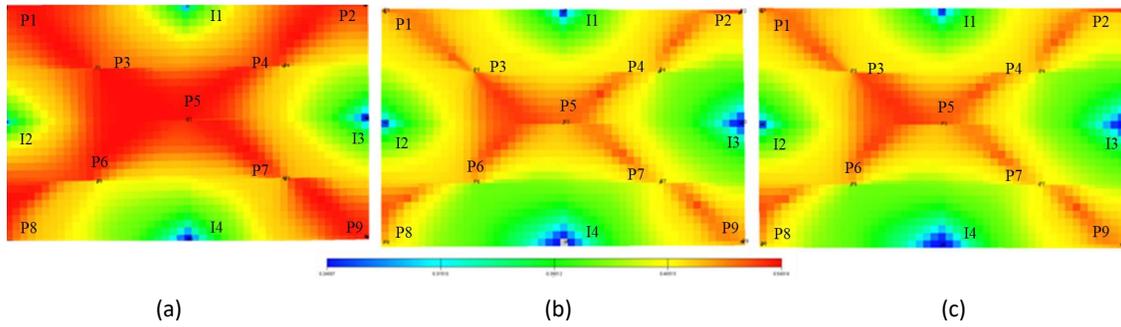


Fig. 12. Residual saturation of the edge well, (a) the 4th year before refracturing, (b) the 10th year without refracturing, (c) the 10th year, refracturing at the 4th year without fracture reorientation.

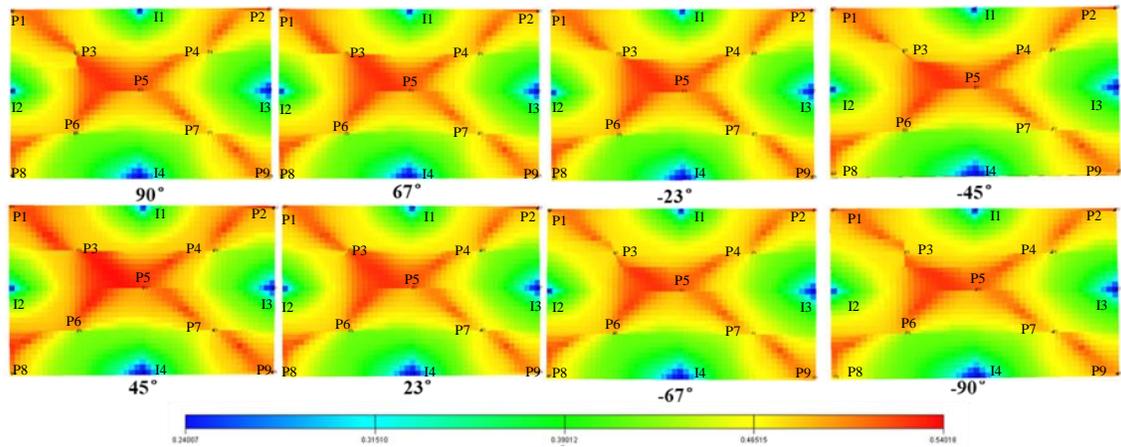


Fig. 13. Oil saturation with different angles of fracture reorientation after refracturing (edge well).

Table 2. Cumulative oil production of different refracture propagation direction (corner well).

Angles	Accumulative oil production/10 ⁴ m ³
-90°	1.363
-67°	1.328
-45°	1.308
-23°	1.364
0°	1.225
23°	1.352
45°	1.281
67°	1.295
90°	1.331
No refracturing	0.949

Cumulative oil production of target corner wells with different angles of fracture reorientation is obtained as shown in Table 2.

Based on analysis of residual oil distribution of corner wells, residual oil motivated in the later 6 years after refracturing differs with different reoriented angles. As shown in Fig. 14, accumulative oil production with different angles of frac-

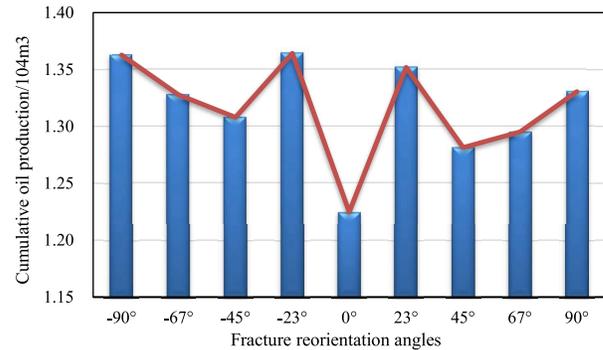
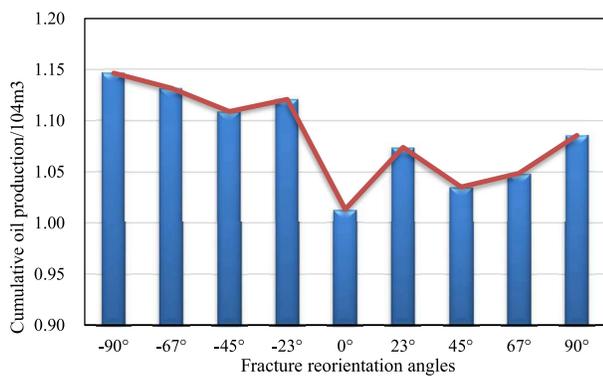


Fig. 14. Cumulative oil production of different refracture propagation direction (corner well).

ture are obviously different, which are higher at the angle of positive and negative 23°, as well as positive and negative 90°. Also, it is obviously that there is some kind of relationship among angles in positive and negative angles, both of which have the highest production with angle of 23°, then 90°, 67° and with 45° at the lowest. However, production of positive angles is higher than the same angle at the positive angle which is caused by the heterogeneity of the reservoir properties. Properties such as permeability and porosity at the upper part of the model are better than those of the lower part, which is

Table 3. Cumulative oil production of different refracture propagation direction (edge well).

Angles	Accumulative oil production/ 10^4 m^3
-90°	1.147
-67°	1.132
-45°	1.109
-23°	1.121
0°	1.013
23°	1.074
45°	1.035
67°	1.048
90°	1.086
No refracturing	0.847

**Fig. 15.** Cumulative oil production of different refracture propagation direction (edge well).

shown as more residual oil produced at the early term of development. So, more residual oil will be produced because of fracture reoriented to those regions at lower part after refracturing.

5.2 Enhanced oil recovery of edge well

Cumulative oil production of target edger wells with different angles of fracture reorientation is obtained as shown in Table 3 and plotted in Fig. 15.

Based on analysis of residual oil distribution of edge wells, residual oil motivated in the later 6 years after refracturing differs with different reoriented angles. As shown in Fig. 16, accumulative oil production with different angles of fracture is obviously different, but production is higher at the positive angle than that at the negative angles different with that of corner well. The reason of the difference between corner well and edge well is obviously due to the well position in the well pattern. Same as the corner well, there is some kind of relationship among angles in positive and negative angles, both of which have the high production with angle of 90° and 23° , then 67° and 45° , and also with 45° at the lowest.

Results show that for corner wells, the optimal angles for fracture reorientation are positive and negative 23° , while for edge well, the optimal angles are positive and negative 90° .

As discussed above, well pattern, well position, fracture reoriented angle and reservoir properties are all important factors for evaluating potential of refracturing.

6. Conclusions

Mechanisms of fracture reorientation is discussed and feasibility of fracture reorientation can be predicted by the criteria presented. Based on the numerical simulation results, residual oil distribution with reoriented fractures is discussed and the estimated ultimate recovery is predicted.

(1) Mechanical effect and poroelastic effect are the two main factors for stress field change which lead to formation of stress reversal region and initiation of fracture reorientation.

(2) The two dimensionless criteria can reveal mechanical effect and poroelastic effect and help to identify the possibility of fracture reorientation. Reorientation is easy to happen in wells with either small mechanical stress reorientation number or poroelastic stress reorientation number.

(3) Distribution of residual oil with different fracture angles is obviously different and there is also difference for wells at different position in the well pattern, like corner well and edge well.

(4) Potential of enhancement is significantly different with angles of fractures which is shown as: cumulative produced oil of the corner well is symmetrical around the angle of 0° from positive and negative for both corner well and edge well. The optimal angles for fracture reorientation are positive and negative 23° , while for edge well, the optimal angles are positive and negative 90° .

(5) Well pattern, well position, fracture reoriented angle and reservoir properties are all important factors for evaluating potential of refracturing which should be considered before restimulation design.

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Conflict of interest

The authors declare no competing interest.

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